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Comparison of mechanical properties and microstructural characterization of CoCrMo alloy obtained via selective laser melting (SLM) and casting technique <u>M. V. Mergulhão¹, C. E. Podestá^{1,2}, M. D. M. Neves¹</u>

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Abstract

Advances in processes using the powder metallurgy techniques are making this technology competitive compared to the other traditional manufacturing processes, especially in medicine area. The additive manufacturing technique – selective laser melting (SLM) was applied in a biomaterial of CoCrMo alloy (ASTM F75), to study the mechanical properties and microstructural characterization in comparison between the conventional technique – lost wax casting. Yet there is an important knowledge of performance properties, dimensional, mechanical and microstructural of this sintered alloy compared to casting, as reported recently (MERGULHÃO et al., 2015a, 2015b; PODESTÁ et al., 2015). The aim of this study is to demonstrate the mechanical properties and microstructures of specimens manufactured by powder metallurgy techniques using the SLM, using the Co-Cr-Mo alloy in the form of particulate matter.

Mechanical curves of uniaxial stress are presented at Figure 3 and for more explanations about the mechanical properties values is apresented at the Table 3.



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Materials and Methods

The Co-Cr-Mo alloy gas atomized (H.C Starck® Company) was provided by the HighBond company in three different particle sizes (granulometric range), respectively by terminologies D1 < 15 μ m, D2 15-45 μ m and D3 76-106 μ m. The confirmation of the chemical composition by fluorescence spectrometer X-ray energy dispersive of powders is presented in Table 1.The flow chart of the process of this study is showed in Figure 1.

Table 1 – Chemical composition (weight %) of Co-Cr-Mo powder and the standard reference ASTM F75.

	Cobalt	Chromium	Molybdenum	Iron
Powder	$63,\!86 \pm 0,\!07$	$28,\!96\pm0,\!04$	$7,02 \pm 0,01$	$0,16 \pm 0,01$
Cast	$62,\!601 \pm 0,\!06$	$27,\!998 \pm 0,\!04$	$6,02 \pm 0,01$	$0,213 \pm 0,01$
ASTM F75	Balance	$30,00 - 27,00 \pm 0,30$	7,00 - 5,00 \pm 0,15	$0,\!75\pm0,\!03$



0 0,5 1 1,5 2 2,5 3 3,5 4

STRAIN OF CROSSHEAD [mm] Figure 3 – Stress curves of specimens – cast (Cp C) and selective laser melting (Cp SLM).

Table 3 – Mechanical properties (medium values and desviations) of the specimens manufactured by casting and SLS process. (NU= not usual)

Reference	Туре	0.2% YS [MPa]	Elongation [%]	E [GPa]	UTS [MPa]	TRS [MPa]	HV [0.1mN/10s]
Co-Cr-Mo alloy	CAST	$276,20 \pm 43,60$	$8,37 \pm 4,45$	291,21 \pm 15,22	453,62 ± 75,91	NU	$365,74 \pm 16,15$
	SLM	$731,50 \pm 40,31$	$13,73 \pm 5,32$	$276,70 \pm 12,63$	$1136,95 \pm 0,92$	$1127,91 \pm 0,15$	$420,62 \pm 21,16$
ISO 22674:06	1	80	18		_	_	_
	2	180	10				
	3	270	5	-			
	4	360	2				
	5	500	2	150			
ASTM I	F 75	450	8	-	655	-	253-327 HV

The microstructure and the fractures of the specimens were evaluated by OM and SEM-EDS as showed in Figure 4 and Figure 5.



Figure 1 – Flow chart of the process of this study and images of tests and specimens.

Results

The results of all physical properties are showed at the Table 2 and the spherical powders analysed by SEM-EDS in Figure 2. The spherical powders presented satellites and the cross-sectioned powder a dendritic characteristic morphology of gas atomization.

Table 2 – Physical properties of Co-Cr powders.

Physical Properties		Powder			
		D1	D2	D3	
	Diameter 10%	5,67	20,88	-	
Granulometric	Diameter 50%	12,73	31,11	-	
Distribuition [µm]	Diameter 90%	19,64	46,10	-	
	Medium Diameter	12,76	32,36	92,81	
Flow Time [s/50g]		-	$15,85 \pm 0,11$	$22,89 \pm 0,03$	
Apparent Density [g/cm ³]		$4,12 \pm 0,01$	$4,51 \pm 0,01$	$4,55 \pm < 0,01$	
Tap Density [g/cm ³]		$5,00 \pm 0,02$	$5,26 \pm 0,05$	$5,09 \pm 0,02$	
Theorical Density (g/cm ³)		8,37			
Pycnometer Density by Helium (g/cm ³)		$8,28 \pm 0,001$	$8,30 \pm 0,001$	$8,27 \pm 0,001$	
Specific Surface (m ² /g)		0,66757	0,01114	0,35287	

Figure 4 – OM and SEM micrographies of CoCrMo a) and b) as-cast sample, c) and d) as-SLM sample and e) and f) respectively semi-quantitative analysis by EDS of samples.



Figure 5 – SEM images of tensile fractures, a) cast sample and b) SLM sample.

To determine the porosity of the consolidated samples was established the density comparison via Helium picnometry between the theoretical density. The results of analysis are shown in the Table 3.

Table 3 – Results (mean and desviations) of porosity analysis methods applied in specimens Co-Cr-Mo.

a •	Density methods [g/cm ³]		
Specimens	Helium Picnometry	Theorical	
CAST	$8,193 \pm 0,007$	9 27	
SLM	$8,244 \pm 0,006$	0,37	

Conclusions

The SLM technique allowed obtaining samples with superior mechanical properties of the cast technique. In this case, the yield strength and elongation were respectively 69,73% and 39,04% greater than the yield strength and elongation obtained in the cast samples. The microstructural characterization of the casting samples showed formation of rich carbide molybdenum. The SLM allowed to obtain samples with improved chemical homogeneity over the molten sample, as discussed in the microstructural characterization of the samples and confirmed by fracture analysis.



Figure 2 – a) to c) SEM micrographs of atomized powders, respectively D1, D2 and D3 granulometric distribution, d) SEM micrograph of cross-sectioned powder etched and e) EDS of powder gas atomized. The processing using laser sintering proved superior to casting processing technique, allowing the use of this technique in the manufacturing area of prosthetics and dental implants.

Acknowledgments

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References

ASTM. Standard Test Method for Transverse Rupture Strength of Powder Metallurgy (PM) Specimens. West Conshohocken: ASTM, 2012. (ASTM B528-12). ISO. Dentistry — Metallic materials for fixed and removable restorations and appliances. Geneva: 2006. (ISO 22674:2006(E)). ASTM. Standard Test Method for Transverse Rupture Strength of Powder Metallurgy (PM) Specimens. West Conshohocken: ASTM, 2012. (ASTM B528-12). MPIF . Standard methods for determination of apparent density of free-flowing metal powders using the Hall apparatus. Princeton: MPIF, 1985. (MPIF Standard 04). MPIF. Standard methods for determination of flow rate of free-flowing metal powders using the hall apparatus. Princeton: MPIF, 1988. (MPIF Standard 03) MPIF. Standard methods for determination tap density of metal powders. Princeton: MPIF, 1985. (MPIF Standard 03) MPIF. Standard methods for determination tap density of metal powders. Princeton: MPIF, 1985. (MPIF Standard 46).

Obtained by Selective Laser Sintering (SLS) and Casting Techniques. Mangaratiba - RJ, 2015a.

Mergulhão, M. V.; Podestá, C. E.; Neves, M. D. M. Das. Mechanical Properties and Microstructural Characterization of Cobalt-Chromium (CoCr) Sintered Obtained by Casting and Selective Laser Sintering (SLS). Mangaratiba - RJ, 2015b.

Podestá, C. E.; Mergulhão, M. V.; Neves, M. D. M. Das. Comparative Study of Mechanical Properties Between Casting and Selective Laser Sintering (SLS) in Cobalt Chromium Alloys. San Diego, 2015.