

1 **Production of high melt strength polypropylene by gamma irradiation.**

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10
11 **Abstract**

12 High melt strength polypropylene (HMS-PP) have been recently developed and
13 introduced in the market by the major international producers of polypropylene. Therefore,
14 BRASKEM the leading Brazilian PP producer together with EMBRARAD the leading
15 Brazilian gamma-irradiator and the IPEN's polymer group worked to developed a national
16 technology for the production of HMS-PP. One of the effective approaches to improve melt
17 strength and extensibility is to add chain branches onto polypropylene backbone using
18 gamma radiation. Branching and grafting result from the radical combinations during
19 irradiation process. Crosslinking and main chain scission in the polymer structure are also
20 obtained during this process. In this work gamma irradiation technique was used to induce
21 chemical changes in commercial polypropylene with two different monomers, Tri-allyl-
22 isocyanurate (TAIC) and Tri-methylol-propane-trimethacrylate (TMPTMA), with
23 concentration ranging from 1.5 to 5.0 mmol/100g of polypropylene. These samples were
24 irradiated with a ⁶⁰Co source at dose of 20kGy. It were used two different routes of HMS-PP
25 processing. The crosslinking of modified polymers was studied by measuring gel content;
26 melt flow rate and rheological properties like melt strength and drawability. It was observed
27 that the reaction route and the monomers type have influenced the properties; however the
28 concentration variation of monomer has no effect.

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30 **Keywords:** *Polypropylene; gamma radiation; crosslinking and melt strength.*

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36 **Introduction**

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38 There are many technologies to produce polypropylene (PP) with controlled
39 rheological behavior especially in the case of elongational flow¹⁻⁶. The modification of
40 polypropylene can be made through *in situ* polymerization, using metallocene catalysts,
41 electron or gamma irradiation in the presence of polyfunctional monomers or by different
42 methods of degradation. In the last case, the more prominent method is used the distinct
43 peroxides to promote degradation of polypropylene during extrusion, also termed vis-
44 breaking, as a well recognized manufacturing process¹⁻⁴. Degradation of PP with peroxides
45 is believed to occur by a series of free-radical reactions involving steps as initiation,
46 scission, transfer and termination. These steps processes have been observed when polymers
47 were irradiated with high energy radiation⁷. Degradation process, generally converts the low
48 melt flow index (MFI) commodity resins to high MFI resins with superior processing
49 properties, but reducing viscosity and elasticity this final material has poor mechanical
50 properties.

51 The isotactic polypropylene (iPP) is a typical thermoplastic with a number of
52 desirable basic properties that make it a versatile material among thermoplastics. These
53 properties coupled with its low specific gravity and low cost are the primary reason for this
54 popularity as a commodity resin. However, its linear structure leads to poor processability
55 involving elongational flow. It's known that the molecular weight and molecular weight
56 distribution (MWD) determine the rheological properties of polypropylene melts. These
57 parameters must be controlled to get better material response during processing and to
58 achieve the diversity in polymer grades suitable for the different applications. To improve
59 the processability of iPP and to have various grades, the molecular weight and the MWD
60 can be modified in a post-reactor operation by means of different methods¹⁻⁷. In the case of
61 iPP the presence of long chain branching or grafting strongly affect the molar weight and
62 MWD.

63 The radiation process has played an important role to produce polymers with these
64 controlled rheological properties. The irradiation of polymeric materials with ionizing
65 radiation (accelerated electrons, X-rays, ion beams, gamma rays) leads to the formation of
66 very reactive free radicals intermediate, ions and excited states. These intermediates can
67 follow several reaction paths results in the new bonds formation, as well as in the case of
68 peroxide degradation process. The transformation degree (extension) depends on the
69 structure of the polymer and the conditions of pre treatment, during and after irradiation as

70 well as dose rate. The modification of polymers by irradiation cover crosslinking, induced
71 polymerization (graft polymerization and curing) and degradation. The success of radiation
72 technology for the processing of synthetic polymers can be attributed to two reasons,
73 namely the easiness of processing in various shapes and sizes and, secondly, most of these
74 polymers undergo crosslinking reaction upon exposure to radiation. A significant difference
75 exists between electron beam and gamma processing of polymers, which is related to dose
76 rate and often to oxidative degradation of material at or near the surface for reactions
77 conducted at low dose-rates^{1,5-7}.

78 Actually, there are different interests for development of polypropylene with long
79 branching or grafting, the new family of polypropylene called high melt strength
80 polypropylene (HMS-PP). First of all, the transient elongational viscosity is very important
81 for a description of process involving elongational deformation such as film blowing, blow
82 molding or thermoforming. On the other hand, elongational behavior is a sensitive indicator
83 of properties concerning the molecular structure such as high molecular weight tails or long-
84 chain branching and in some cases were influenced the existence of crosslinking and
85 degradation. The influence of molecular structure of the melt on the spinning (Rheotens
86 tests) and uniaxial elongational viscosity were described and studied by many authors^{1,4,5,8-}
87 ¹⁰. Branching and crosslinking have strong effects on the rheological properties of the
88 material in the molten state. In order to measure these effects the Rheotens tests has been
89 used. In this test an extruded filament was subjected to elongational deformation under the
90 action of a tensile force and the drawdown force need for extension of an extruded melt
91 strand was measured as a function of drawdown velocity. The melt strength was considered
92 as the drawdown force required to break the melt strand⁸⁻¹⁰.

93 In the present work it were studied two routes to produce branching and grafting
94 polypropylene (with rheological behavior controlled) using gamma irradiation and
95 multifunctional monomers. In this case two kind of monomers were investigated: Tri-allyl-
96 iso-cyanurate (TAIC) and Tri-methylolpropane-trimethacrylate (TMPTMA) with
97 concentration ranging from 1.5 to 5.0 mmol/100g of polypropylene. These samples were
98 irradiated at dose of 20kGy. The gel fraction, MFI and rheological analysis (elongational
99 flow and drawability) have been performed, trying to extrapolate from these data the
100 differences between the various monomers, their concentration routes of process.

101

102 **Experimental**

103 **Material and Sample Preparation**

104 The polypropylene used in this work was obtained from Braskem. This material
105 showed a melt flow index of 1.5 g/10 min, determined using ASTM D 1238 (230°C and
106 2.16 kg). The polyfunctional monomers studied were *Tri-allyl-iso-cyanurate* (TAIC) and
107 *Tri-methylolpropane-trimetacrylate* (TMPTMA), supplied by *Cytec* and *Sartomer*
108 *Industries*, respectively. Both monomers are trifunctional and were used as received.

109 Monomers at a concentration of 1.5 to 5.0 mmol/100g of iPP were mixed at room
110 temperature (route 1) and in the second case submitted to higher temperature mixing (route
111 2). After that, all samples were irradiated with gamma radiation (⁶⁰Co) at dose of 20 kGy
112 under nitrogen gas atmosphere.

113

114 **Gamma Irradiation**

115 The samples were irradiated at Embrarad with a ⁶⁰Co source, at a dose rate of
116 10 kGy/h and the dosimetry was performed with Harwell Red Perspex 4034.

117

118 **Gel content measurements**

119 Gel content was measured using a standard method ASTM D2765. Samples of iPP
120 modified were weighed, placed in bags and extracted with xylene as solvent (i.e. refluxing)
121 for 24 hours at temperature of 130°C. After that, the extracts were removed, dried under
122 vacuum for 24 hours until to constant weight and weighed to determine the gel fraction
123 according to equation 1:

$$124 \text{ Gel fraction (\%)} = (W/W_0) \cdot 100 \quad (1)$$

125 where W and W₀ are the weights of the dried samples after and before the extraction
126 procedure respectively.

127

128 **Melt flow index**

129 The melt flow rate of the modified polypropylenes by two routes of process was
130 measured in a Melt flow Junior equipment Mod 09237 in which the samples were flowed
131 through an orifice of 2.00 mm diameter during 10 min under a loading of 2.16 Kg at 230°C
132 (ASTM D 1238).

133

134 **Rheotens test**

135 In the Rheotens test the tensile force needed for elongation of an extruder polymer
136 filament was measured as a function of the draw ratio. The polymer was extruded in a
137 Haake rheometer (screw diameter of the 2.0 mm) in combination with a Rheotens Mod.

138 71.97 apparatus manufactured by Göttfert. The extrusion melt temperature was 190°C and
139 the die velocity varied between 40.0 at 575.0 mm.s⁻¹. It can be assumed that cooling of the
140 extruded strand in the spinline is small, so the polymer melt is elongated under isothermal
141 conditions.

142

143 **Results and discussion.**

144

145 The crosslinking degree, during the process of modification of iPP was estimated by
146 gel content. In the Figure 1 is possible observed the gel fraction behavior of two sets of
147 samples starting from two routes of process for TAIC and TMPTMA monomers in a large
148 range of concentrations. These data were compared with the date for the pure polymer. It
149 can be seen that, there was no change in the gel fraction of the samples produced by the
150 route 1 in comparison with the pure iPP and the samples obtained by route 2. On the other
151 hand, the increases of monomers concentration increase the gel fraction obtained by the
152 route 2, except in the case of TAIC at 5.0 mmol. Probably, in this case the chain scissions
153 occur preferentially to the other reactions, for example, grafting or crosslinking. In the route
154 2, the TAIC strongly react with the iPP chains modifying the structure in comparison with
155 TMPTMA, showed by high values of gel fraction.

156

Insert Figure 1

157 In general, the increase of entanglement in the melt state from the introduction of
158 branching or crosslinking carry out a decrease of melt flow rate. The values of MFI of the
159 samples as a function of monomer concentration at each process route is showed in the
160 Figure 2. The samples obtained by route 2 showed the smaller MFI value than that of the
161 route 1 corroborating with the gel fraction value, high gel fraction lead to low MFI. But, the
162 rise in the monomer concentration led to a decrease in the MFI for route 1 and practically no
163 change was observed for samples obtained by route 2 (except for case of TMPTMA 3.0
164 mmol).

165

Insert Figure 2

166 Figures 3 shows the force at which the melt polymer breaks that corresponds to the
167 melt strength for all the samples of modified polypropylene as a function of monomer
168 concentration. Polypropylene modified via route 2 exhibit high values of melt strength for
169 TAIC and TMPTMA. The measurement of the melt strength was not possible in the case of
170 iPP with TAIC 5.0 mmol due to the high crosslinking degree of the material. On the other
171 hand, route 1 showed lower values of melt strength and smaller than pure iPP. In this routes

172 the degradation process (chain scission) may be dominant over grafting or branching
173 phenomenon.

174 **Insert Figure 3**

175

176 The extensibility of iPP modified melt has been determined by the rheotens testes
177 and can be defined as the drawdown force needed for elongation of an extruded strand and
178 is measured as a function of slowly increasing drawdown speed. In the Figure 4 it can be
179 observed the maximum drawdown velocity until the break of polymer filament for all
180 samples as a function of monomer concentration. It was observed that samples with high
181 values of melt strength show small drawdown velocity (route 2). However, samples
182 produced by the route 1 the drawability is higher when compared with pure iPP and the
183 samples prepared by the route 2. This behavior may be ascribed to the dependence of iPP
184 melt strength on its molecular weight, polydispersivity, degree of branches and
185 entanglement density. However, the melt extensibility probably depends on the existence of
186 a high level of molecule entanglements. In other words, drawability arises from higher
187 degradation process (see Figure 2).

188

Insert Figure 4

189 **Conclusion.**

190

191 Gamma-irradiation was successfully used to alter the molecular structure of linear
192 polypropylene. The utilization of polyfunctional monomers TAIC and TMPTMA as a
193 crosslinking agents lead to modification of iPP structure in the two applied routes of
194 process. Evidence of this was found in the form of insoluble gel contents in the samples, as
195 well as a variation on the melt flow rates. Higher concentration of monomers led to samples
196 with a greater melt strength, especially in the route 2 in comparison to the route 1. But the
197 drawability was dropped for all cases with the variation of monomer concentration.
198 Different steps during process to obtain modified linear polypropylene pos-reactor influence
199 the rheological properties of final product. In the irradiation of a polymer there is always a
200 balance between crosslinking, branching and degradation reactions mechanisms influenced
201 by chemicals presence. Modifications on the molecular structure area a result of these
202 chemicals and reaction mechanisms.

203

204 **Acknowledgements**

205

206 The authors wish to thank Braskem for polypropylene samples and for the
207 measurements of melt strength and drawability of the modified PP. Embrarad is also
208 acknowledged for performing the gamma irradiation process and finally to FAPESP for the
209 financial support (process number: 02-13070-2 and 04-00383-8).

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236

237 Figure 1 – Dependence of gel fraction of the modified polypropylene on the monomer
238 content for two routes of synthesis. Radiation dose of 20 kGy.

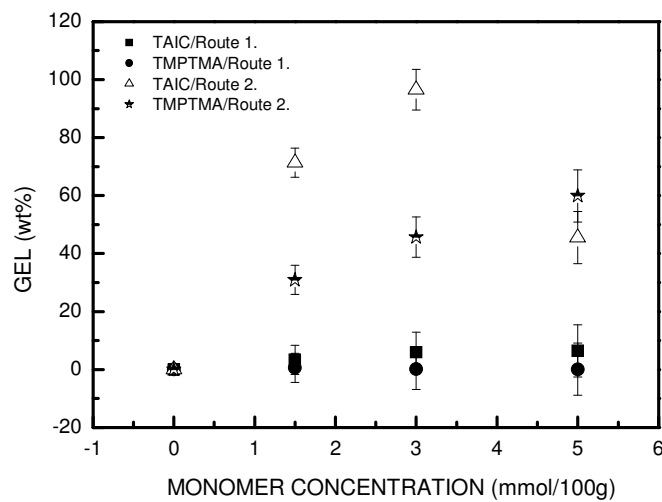
239 Figure 2 – Dependence of MFR of the modified polypropylene on the monomer content for
240 two routes of syntheses. Radiation dose of 20 kGy.

241 Figure 3 – Melt strength of modified polypropylene in dependence of the monomer
242 concentration at 190°C. Radiation dose of 20 kGy.

243 Figure 4 – Draw down velocity at 190°C as a function of monomer concentration of
244 modified polypropylene. Radiation dose of 20 kGy.

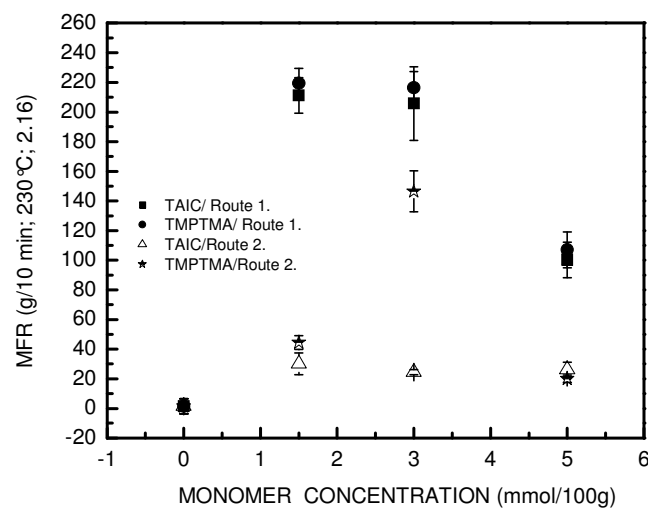
245

246 Fig. 1



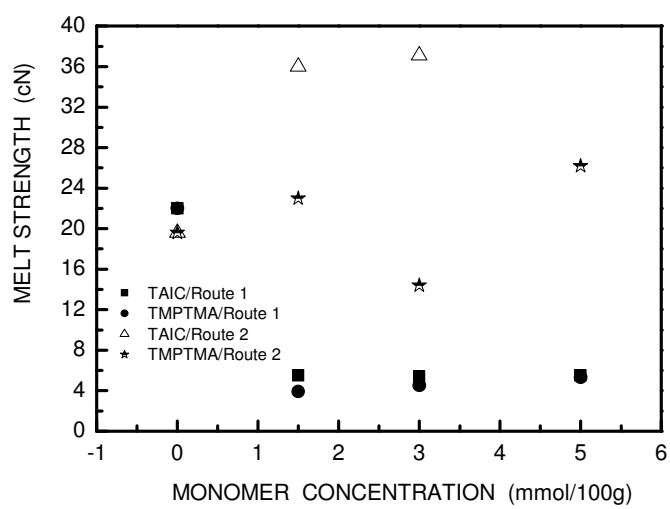
247

248 Fig.2



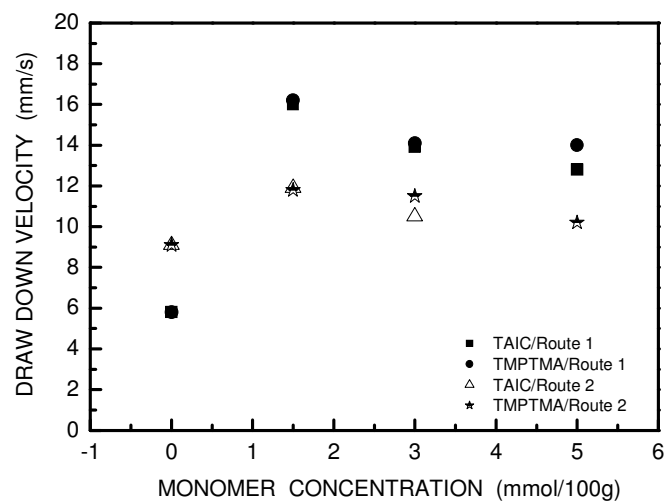
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250 Fig. 3



251

252 Fig.4



253